

Control Systems And Their Components (EE391)

Lec. 9: Closed loop SS Control (Full state feedback)

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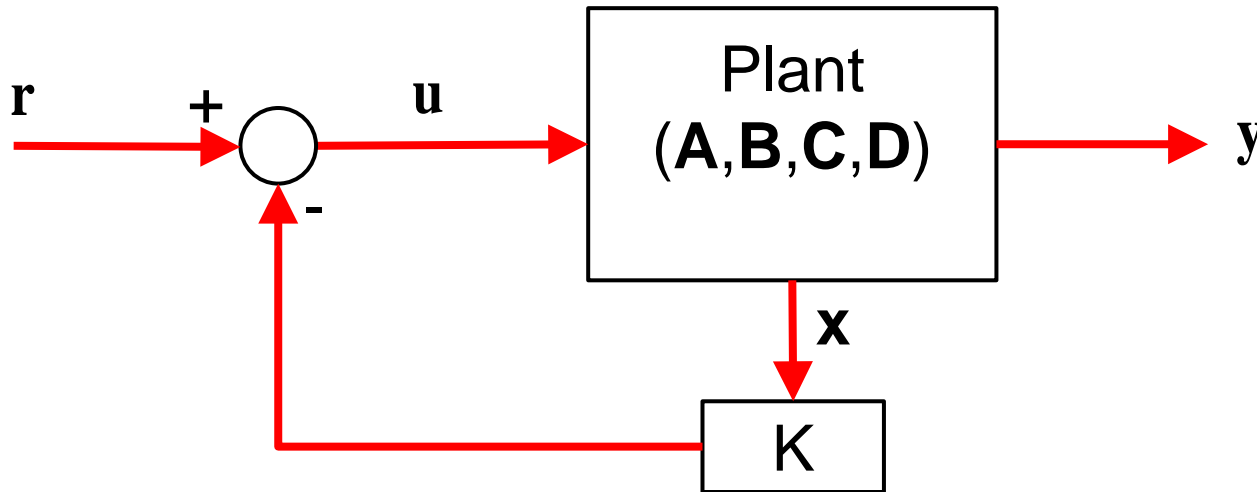
Lecture Outline

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- ❑ Closed loop SS control (why feedback?)
- ❑ Full State feedback (Pole placement technique)
- ❑ Akermann's formula
- ❑ Where to place the poles of closed loop system (Two MATLAB examples)

Closed loop SS control

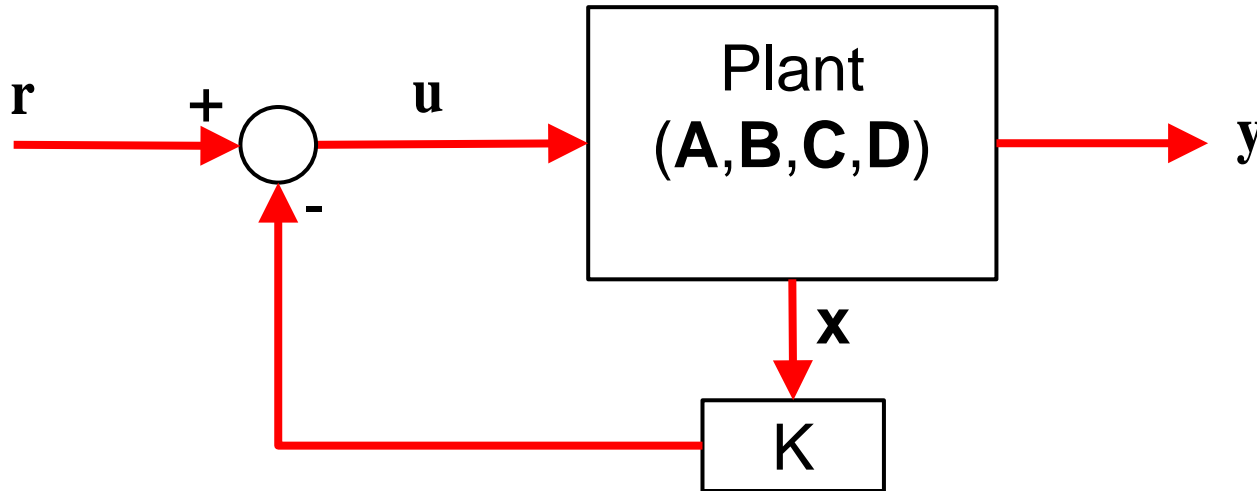
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- Problems with open loop control
 - Impacted by variations of plant model (Not robust)
 - Impacted by external disturbance or noise
 - No control over the transient behavior of system (determined by eigenvalues of $A \rightarrow$ poles of TF)
- With closed loop SS control, we will control the transient behavior of system by modifying poles of TF or eigenvalues of A through **pole placement technique**
- Full state feedback assumes input is linear combination of state variables that are fed back \rightarrow assumes \mathbf{x} is fully measured

Closed loop SS control

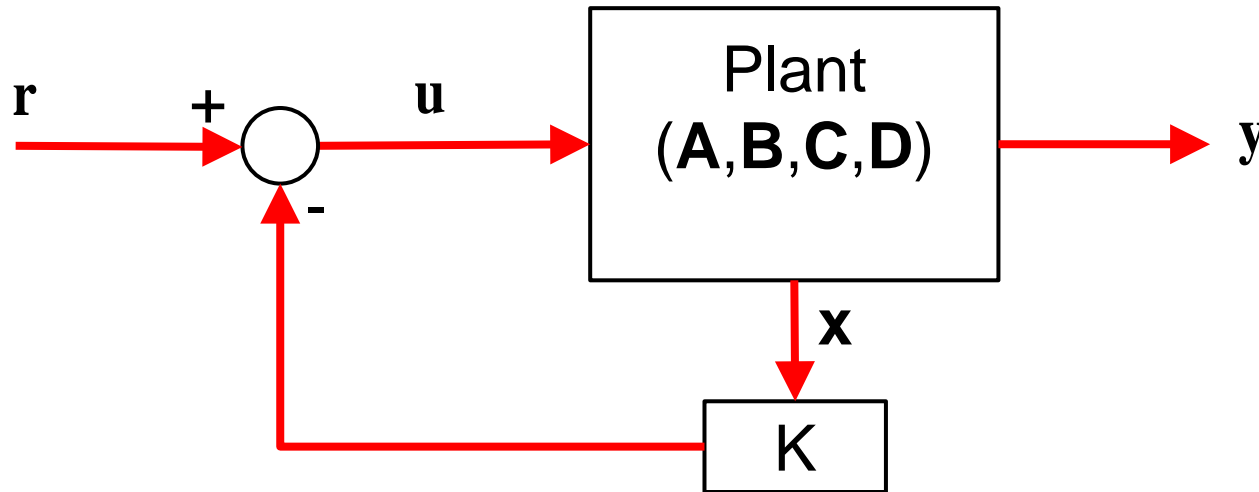
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- Full state feedback assumes input is linear combination of state variables that are fed back → assumes \mathbf{x} is fully measured
- This means I have access over state variables of system
- This is not true!! since the state variables are internal and I only have access to the outputs which I can observe
- We will deal with drawback of full state feedback later by using **state estimators/observers**

Closed loop SS control

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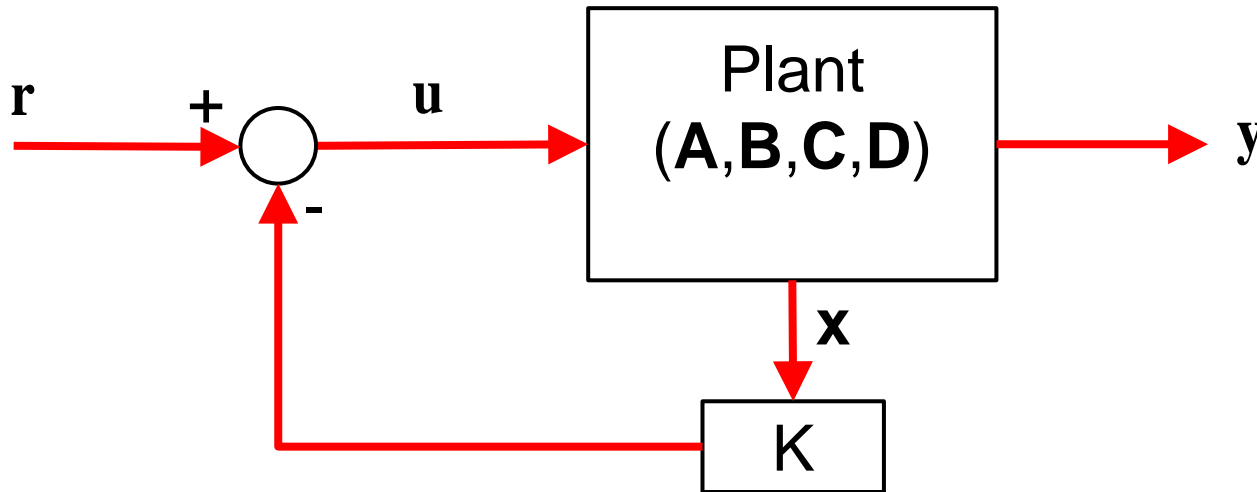


Important Note

In order to be able to perform full state feedback control, the system must be controllable (makes sense but will show up mathematically later on)

Full state feedback

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$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t)$$

Assume full state feedback of the form

$$\mathbf{u}(t) = \mathbf{r}(t) - \mathbf{K}\mathbf{x}(t)$$

where \mathbf{r} is a reference input and $\mathbf{K} \in \mathbf{R}^{1 \times n}$ (assume a single input for simplicity)

Full state feedback

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$$\dot{\mathbf{x}}(t) = (\mathbf{A} - \mathbf{BK}) \mathbf{x}(t) + \mathbf{B}\mathbf{r}(t)$$

Now let us also assume a zero reference input for the moment $\mathbf{r} = 0$ (called regulator)

$$\dot{\mathbf{x}}(t) = (\mathbf{A} - \mathbf{BK}) \mathbf{x}(t)$$

$$\mathbf{A}_{cl}$$

This is the matrix \mathbf{A} for the overall closed loop system with feedback

$$\mathbf{x}(t) = e^{\mathbf{A}_{cl}t} \mathbf{x}(0)$$

The dynamics of the closed loop system is determined by the eigenvalues of \mathbf{A}_{cl} (same as before) and we can choose \mathbf{K} to set them anywhere we want

Full state feedback

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$$|s\mathbf{I} - \mathbf{A}_{cl}| = |s\mathbf{I} - (\mathbf{A} - \mathbf{BK})| = \prod_{j=1}^n (s - s_j) = 0$$



Desired pole locations
of closed loop system

- We start with examples where the desired pole locations are given
- We will then address the issue of how to choose the desired pole locations of closed loop system from required transient specifications given (rise time, maximum overshoot, ...)

Full state feedback

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Example

Find the feedback gains \mathbf{K} of the following SS system such that the closed loop poles become $-2+2i$ and $-2-2i$

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \mathbf{u}(t)$$

Solution

$$\left| sI - \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} k_1 & k_2 \end{bmatrix} \right| = (s + 2 - 2i)(s + 2 + 2i)$$

$$\left| \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ k_1 & k_2 \end{bmatrix} \right| = s^2 + 4s + 8$$

Full state feedback

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Example

Find the feedback gains \mathbf{K} of the following SS system such that the closed loop poles become $-2+2i$ and $-2-2i$

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \mathbf{u}(t)$$

Solution

$$\left| \begin{bmatrix} s & -1 \\ 1+k_1 & s+1+k_2 \end{bmatrix} \right| = s^2 + 4s + 8$$

$$s^2 + (1+k_2)s + (1+k_1) = s^2 + 4s + 8$$

$$1+k_2 = 4 \quad \Rightarrow \quad k_2 = 3$$

$$1+k_1 = 8 \quad \Rightarrow \quad k_1 = 7$$

MATLAB

$\mathbf{K} =$
place(A,B,desired
poles)

Full state feedback

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Example

Find the feedback gains \mathbf{K} of the following SS system such that the closed loop poles become -1, -2, -4

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -3 & 2 & -5 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \mathbf{u}(t)$$

Solution

Eigenvalues of \mathbf{A} of open loop system (without feedback) are -5.467, $0.23+0.7i$, $0.23-0.7i$ \rightarrow The system is not stable

We will make the system stable by placing the poles at desired locations -1, -2, -4 using feedback

Full state feedback

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Example

Find the feedback gains \mathbf{K} of the following SS system such that the closed loop poles become -1, -2, -4

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -3 & 2 & -5 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \mathbf{u}(t)$$

Solution

$$\left| sI - \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -3 & 2 & -5 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} [k_1 \quad k_2 \quad k_3] \right| = (s+1)(s+2)(s+4)$$

$$\left| \begin{bmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 3+k_1 & -2+k_2 & s+5+k_3 \end{bmatrix} \right| = s^3 + 7s^2 + 14s + 8$$

Full state feedback

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Example

Find the feedback gains \mathbf{K} of the following SS system such that the closed loop poles become -1, -2, -4

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -3 & 2 & -5 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \mathbf{u}(t)$$

Solution

$$\left| \begin{bmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 3+k_1 & -2+k_2 & s+5+k_3 \end{bmatrix} \right| = s^3 + 7s^2 + 14s + 8$$

$$s^3 + (5+k_3)s^2 + (k_2-2)s + (3+k_1) = s^3 + 7s^2 + 14s + 8$$

$$\Rightarrow k_1 = 5, k_2 = 16, k_3 = 2$$

Full state feedback

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Note

Last two examples were easy because \mathbf{A}, \mathbf{B} were in controller canonical form. Let's see another example not in CCF and see how things will become a bit complicated

Example

Desired closed loop poles are $-2+2i$ and $-2-2i$, Find \mathbf{K}

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 1 & 1 \\ 1 & 2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \mathbf{u}(t)$$

Solution

$$\left| s\mathbf{I} - \begin{bmatrix} 1 & 1 \\ 1 & 2 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} k_1 & k_2 \end{bmatrix} \right| = (s + 2 - 2i)(s + 2 + 2i)$$

$$\left| \begin{bmatrix} s - 1 + k_1 & -1 + k_2 \\ -1 & s - 2 \end{bmatrix} \right| = s^2 + 4s + 8$$

Full state feedback

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Example

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 1 & 1 \\ 1 & 2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \mathbf{u}(t)$$

Solution

$$s^2 + (k_1 - 3)s + (1 - 2k_1 + k_2) = s^2 + 4s + 8$$

$$k_1 = 7, \quad k_2 = 21$$

We cannot find k 's easily as before by setting each of them to obtain each of the coefficients in the desired polynomial like in CCF (This is one benefit of CCF)

In a system with larger number of state variables we will need to do some algebra to solve for k 's

Full state feedback

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Note

We said that in order to be able to do full state feedback, the system must be controllable → Let's see with an example

Example

Desired closed loop poles are $-2+2i$ and $-2-2i$, find \mathbf{K}

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 1 & 1 \\ 0 & 2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \mathbf{u}(t)$$

Solution

$$\left| s\mathbf{I} - \begin{bmatrix} 1 & 1 \\ 0 & 2 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} k_1 & k_2 \end{bmatrix} \right| = (s + 2 - 2i)(s + 2 + 2i)$$

$$\left| \begin{bmatrix} s - 1 + k_1 & -1 + k_2 \\ 0 & s - 2 \end{bmatrix} \right| = s^2 + 4s + 8$$

Full state feedback

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Example

Desired closed loop poles are $-2+2i$ and $-2-2i$, find \mathbf{K}

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 1 & 1 \\ 0 & 2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \mathbf{u}(t)$$

Solution

$$\left| \begin{bmatrix} s - 1 + k_1 & -1 + k_2 \\ 0 & s - 2 \end{bmatrix} \right| = s^2 + 4s + 8$$

$$(s - 1 + k_1)(s - 2) = s^2 + 4s + 8$$

We can only control the eigenvalue (pole) at $s = -1$ by setting k_1 but we cannot control the eigenvalue (pole) at $s = 2$

Check controllability \rightarrow you will find system **uncontrollable**

Akermann's formula

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- It gives a formal way to obtain \mathbf{K} in full state feedback control all in one step
- Without proof

$$\mathbf{K} = \begin{bmatrix} \phi_0 & \phi_1 & \dots & \phi_{n-1} \end{bmatrix} \mathbf{C}_n^{-1} \text{cl} (\quad)$$

Controllability
matrix

Characteristic equation
of closed loop system
for $s = \mathbf{A}$

- Clearly \mathbf{C}_n needs to be invertible, hence full rank, hence the system must be **controllable**

Akermann's formula

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Example

Use Akermann's formula to find \mathbf{K} of the following SS system \rightarrow closed loop poles required are $-2+2i$ and $-2-2i$

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \mathbf{u}(t)$$

Solution

$$\mathbf{C}_n = [\mathbf{B} \quad \mathbf{A}\mathbf{B}] = \begin{bmatrix} 0 & 1 \\ 1 & -1 \end{bmatrix} \Rightarrow \mathbf{C}_n^{-1} = \frac{1}{-1} \begin{bmatrix} -1 & -1 \\ -1 & 0 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 0 \end{bmatrix}$$

$$\Phi_{cl}(s) = s^2 + 4s + 8 \Rightarrow \Phi_{cl}(\mathbf{A}) = \mathbf{A}^2 + 4\mathbf{A} + 8 = \begin{bmatrix} 7 & 3 \\ -3 & 4 \end{bmatrix}$$

$$\mathbf{K} = [0 \quad 1] \begin{bmatrix} 1 & 1 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} 7 & 3 \\ -3 & 4 \end{bmatrix} = [0 \quad 1] \begin{bmatrix} 4 & 7 \\ 7 & 3 \end{bmatrix} = [7 \quad 3]$$

Same as slide 10!!

Where to put the closed loop poles?

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$$|s\mathbf{I} - \mathbf{A}_{cl}| = |s\mathbf{I} - (\mathbf{A} - \mathbf{BK})| = \prod_{j=1}^n (s - s_j) = 0$$



???

- Desired pole locations are found from required transient specifications (Max. overshoot, settling time, rise time, ...)
- Closed form expressions for these specifications in terms of the pole locations are available for 2nd order system
- If our system is second order, we can use these equations directly to find the poles from the specifications
- If our system is larger, we still use the equations of a second order prototype system to find two poles, and place the remaining poles far away from the $j\omega$ axis (at 5-10 times larger than real part of desired poles of 2nd order system) to make sure they do not impact the system transient

2nd order prototype system

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$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

ω_n : natural undamped frequency, ζ : damping ratio

two poles are

$$\zeta\omega_n \pm i\omega_n\sqrt{1-\zeta^2}$$

$$\text{Maximum overshoot} = e^{\frac{-\pi\zeta}{\sqrt{1-\zeta^2}}}$$

$$2\% \text{ settling time} \approx \frac{4}{\zeta\omega_n}, \quad 5\% \text{ settling time} \approx \frac{3.2}{\zeta\omega_n}$$

MATLAB example 1 (2nd order system)

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$$G(s) = \frac{8}{(s - 5)(s - 10)}$$

Maximum overshoot = 5%

2% settling time = 4 sec

- Find the desired two poles
- Find K that achieves so
- Make sure closed loop system satisfy the specifications

MATLAB example 2 (3rd order system)

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$$G(s) = \frac{8}{(s-5)(s-10)(s-7)}$$

Maximum overshoot = 5%

2% settling time = 4 sec

- Find the desired two poles
- Place the remaining pole far away
- Find K that achieves so
- Make sure closed loop system satisfy the specifications