

Control Systems And Their Components (EE391)

Lec. 7: Discrete SS model, Controllability and Observability

Wed. April 13th, 2016

Dr. Mohamed Hamdy Osman

Lecture Outline

2

- ❑ Discrete SS model
- ❑ Solution of discrete SS model (Time evolution)
- ❑ Controllability and observability concepts
- ❑ Mathematical conditions of controllability and observability

Discrete SS model

3

- Importance is because most analog systems are controlled via digital controller
- We will find discrete SS model from the already derived continuous time SS model (Differential Eqs → Difference Eqs)

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t)$$

$$\mathbf{x}(t) = e^{\mathbf{A}t}\mathbf{x}(0) + e^{\mathbf{A}t} * \mathbf{B}\mathbf{u}(t)$$

$$\mathbf{x}(t) = e^{\mathbf{A}t}\mathbf{x}(0) + \int_0^t e^{\mathbf{A}(t-\tau)}\mathbf{B}\mathbf{u}(\tau)d\tau$$

$$\mathbf{x}(t) = \mathbf{\Phi}(t)\mathbf{x}(0) + \int_0^t \mathbf{\Phi}(t-\tau)\mathbf{B}\mathbf{u}(\tau)d\tau$$



State Transition Matrix

$$\mathbf{\Phi}(t) = e^{\mathbf{A}t}$$

Discrete SS model

4

$$\mathbf{x}(t) = \mathbf{\Phi}(t)\mathbf{x}(0) + \int_0^t \mathbf{\Phi}(t - \tau)\mathbf{B}\mathbf{u}(\tau)d\tau$$

put $t = t_0$

$$\mathbf{x}(t_0) = \mathbf{\Phi}(t_0)\mathbf{x}(0) + \int_0^{t_0} \mathbf{\Phi}(t_0 - \tau)\mathbf{B}\mathbf{u}(\tau)d\tau$$

Multiply by $\mathbf{\Phi}^{-1}(t_0) = \mathbf{\Phi}(-t_0)$ and solve for $\mathbf{x}(0)$

$$\mathbf{x}(0) = \mathbf{\Phi}(-t_0)\mathbf{x}(t_0) - \mathbf{\Phi}(-t_0) \int_0^{t_0} \mathbf{\Phi}(t_0 - \tau)\mathbf{B}\mathbf{u}(\tau)d\tau$$

$$\mathbf{x}(0) = \mathbf{\Phi}(-t_0)\mathbf{x}(t_0) - \int_0^{t_0} \mathbf{\Phi}(-\tau)\mathbf{B}\mathbf{u}(\tau)d\tau$$

Back substitute $\mathbf{x}(0)$

Discrete SS model

5

$$\begin{aligned}\mathbf{x}(t) &= \mathbf{\Phi}(t - t_0)\mathbf{x}(t_0) - \int_0^{t_0} \mathbf{\Phi}(t - \tau)\mathbf{B}\mathbf{u}(\tau)d\tau + \int_0^t \mathbf{\Phi}(t - \tau)\mathbf{B}\mathbf{u}(\tau)d\tau \\ &= \mathbf{\Phi}(t - t_0)\mathbf{x}(t_0) + \int_{t_0}^t \mathbf{\Phi}(t - \tau)\mathbf{B}\mathbf{u}(\tau)d\tau\end{aligned}$$

Now set $t_0 = kT$ and $t = t_0 + T$ where T is the sample duration (discrete) to see transition of state variables from one sample to the next

$$\mathbf{x}(kT + T) = \mathbf{\Phi}(T)\mathbf{x}(kT) + \int_{kT}^{kT + T} \mathbf{\Phi}(kT + T - \tau)\mathbf{B}\mathbf{u}(\tau)d\tau$$

Now assume input \mathbf{u} is held constant from kT to $kT + T$ which is called zero order hold (ZOH) $\rightarrow \mathbf{u}(kT + T) = \mathbf{u}(kT) = \mathbf{u}(k)$ and use discrete time index by omitting T

Discrete SS model

6

$$\begin{aligned}\mathbf{x}(k+1) &= \mathbf{\Phi}(T)\mathbf{x}(k) + \left[\int_{kT}^{kT+T} \mathbf{\Phi}(kT+T-\tau)d\tau \right] \mathbf{B}\mathbf{u}(k) \\ &= \mathbf{\Phi}(T)\mathbf{x}(k) + \left[\int_0^T \mathbf{\Phi}(v)dv \right] \mathbf{B}\mathbf{u}(k) \\ &= \mathbf{A}_d\mathbf{x}(k) + \mathbf{B}_d\mathbf{u}(k)\end{aligned}$$

where

$$\mathbf{A}_d = \mathbf{\Phi}(T) = e^{\mathbf{A}T}$$

$$\mathbf{B}_d = \left[\int_0^T \mathbf{\Phi}(v)dv \right] \mathbf{B}$$

For small T



$$\mathbf{A}_d \approx \mathbf{I} + \mathbf{A}T$$

$$\mathbf{B}_d \approx T\mathbf{B}$$

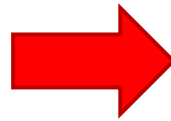
Discrete SS model

7

$$\begin{matrix} n \times 1 & n \times 1 & p \times 1 \\ \dot{\mathbf{x}}(t) = & \mathbf{A} \mathbf{x}(t) + & \mathbf{B} \mathbf{u}(t) \\ & n \times n & n \times p \end{matrix}$$

$$\begin{matrix} m \times 1 & n \times 1 & p \times 1 \\ \mathbf{y}(t) = & \mathbf{C} \mathbf{x}(t) + & \mathbf{D} \mathbf{u}(t) \\ & m \times n & m \times p \end{matrix}$$

Continuous



$$\begin{matrix} n \times 1 & n \times 1 & p \times 1 \\ \mathbf{x}(k + 1) = & \mathbf{A}_d \mathbf{x}(k) + & \mathbf{B}_d \mathbf{u}(k) \\ & n \times n & n \times p \end{matrix}$$

$$\begin{matrix} m \times 1 & n \times 1 & p \times 1 \\ \mathbf{y}(k) = & \mathbf{C}_d \mathbf{x}(k) + & \mathbf{D}_d \mathbf{u}(k) \\ & m \times n & m \times p \end{matrix}$$

Discrete

MATLAB

$[\mathbf{A}_d \ \mathbf{B}_d \ \mathbf{C}_d \ \mathbf{D}_d] =$
`c2dm(A,B,C,D, T,'zoh')`

$$\mathbf{A}_d = e^{\mathbf{A}T} \approx \mathbf{I} + \mathbf{A}T$$

$$\mathbf{B}_d = \begin{bmatrix} T \\ \int_0^T e^{\mathbf{A}v} dv \\ 0 \end{bmatrix} \mathbf{B} \approx T\mathbf{B}$$

$$\mathbf{C}_d = \mathbf{C}$$

$$\mathbf{D}_d = \mathbf{D}$$

Discrete SS model

8

MATLAB problem

- Find the continuous time SS model of the following TF on MATLAB

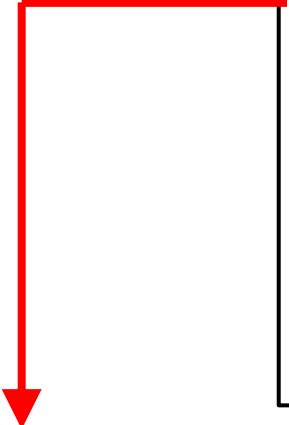
$$G(s) = \frac{2s^2 + 8s + 6}{s^3 + 8s^2 + 16s + 6}$$

- Find discrete time equivalent SS model of the above system

```
[A B C D] = tf2ss([2 8 6],[1 8 16 6])  
[A_d B_d C_d D_d] = c2dm(A,B,C,D,1,'zoh')
```


Solution of discrete SS model

9

$$\begin{array}{l} \overset{n \times 1}{\mathbf{x}(k+1)} = \underset{n \times n}{\mathbf{A}_d} \overset{n \times 1}{\mathbf{x}(k)} + \underset{n \times p}{\mathbf{B}_d} \overset{p \times 1}{\mathbf{u}(k)} \\ \overset{m \times 1}{\mathbf{y}(k)} = \underset{m \times n}{\mathbf{C}_d} \overset{n \times 1}{\mathbf{x}(k)} + \underset{m \times p}{\mathbf{D}_d} \overset{p \times 1}{\mathbf{u}(k)} \end{array}$$


- We are going to call them A, B, C, D for simplicity but it is implicitly known that they are the discrete equivalent of the cont. time A,B,C,D
- We need to solve this difference equation to obtain $\mathbf{x}(k)$ in terms of $\mathbf{x}(0)$ and \mathbf{u}
- We can use Z transform similar to what we did with Laplace transform in the continuous case, or

Solution of discrete SS model

10

$$\mathbf{x}(k + 1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k)$$

$$\mathbf{x}(1) = \mathbf{A}\mathbf{x}(0) + \mathbf{B}\mathbf{u}(0)$$

$$\mathbf{x}(2) = \mathbf{A}\mathbf{x}(1) + \mathbf{B}\mathbf{u}(1) = \mathbf{A}[\mathbf{A}\mathbf{x}(0) + \mathbf{B}\mathbf{u}(0)] + \mathbf{B}\mathbf{u}(1) = \mathbf{A}^2\mathbf{x}(0) + \mathbf{A}\mathbf{B}\mathbf{u}(0) + \mathbf{B}\mathbf{u}(1)$$

$$\begin{aligned}\mathbf{x}(3) &= \mathbf{A}\mathbf{x}(2) + \mathbf{B}\mathbf{u}(2) = \mathbf{A}[\mathbf{A}^2\mathbf{x}(0) + \mathbf{A}\mathbf{B}\mathbf{u}(0) + \mathbf{B}\mathbf{u}(1)] + \mathbf{B}\mathbf{u}(2) \\ &= \mathbf{A}^3\mathbf{x}(0) + \mathbf{A}^2\mathbf{B}\mathbf{u}(0) + \mathbf{A}\mathbf{B}\mathbf{u}(1) + \mathbf{B}\mathbf{u}(2)\end{aligned}$$

$$\mathbf{x}(k) = \mathbf{A}^k \mathbf{x}(0) + \sum_{j=0}^{k-1} \mathbf{A}^{k-1-j} \mathbf{B}\mathbf{u}(j)$$



Similar to state Transition Matrix in discrete case

Solution of discrete SS model

11

Problem

- Try to obtain the same formula using Z transform

$$\mathbf{x}(k + 1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k)$$



$$\mathbf{x}(k) = \mathbf{A}^k \mathbf{x}(0) + \sum_{j=0}^{k-1} \mathbf{A}^{k-1-j} \mathbf{B}\mathbf{u}(j)$$

Problem

- Prove that the TF in discrete case is (similar to continuous)

$$\mathbf{Y}(z) = \left[\mathbf{C}(z\mathbf{I} - \mathbf{A})^{-1} \mathbf{B} + \mathbf{D} \right] \mathbf{U}(z)$$

Controllability concept

12

Illustrative Example

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 3 \\ 0 \end{bmatrix} u(t)$$

$$y(t) = [2 \quad 3] \mathbf{x}(t)$$

- Eigenvalues of \mathbf{A} are -1, -2 (poles of the system)
- Let's find the TF

$$TF = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1} \mathbf{B} + \mathbf{D}$$

$$= [2 \quad 3] \begin{bmatrix} \frac{1}{s+1} & 0 \\ 0 & \frac{1}{s+2} \end{bmatrix} \begin{bmatrix} 3 \\ 0 \end{bmatrix}$$

$$= \frac{6}{s+1}$$

Where is the other pole at -2 ?

Controllability concept

13

Illustrative Example

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 3 \\ 0 \end{bmatrix} u(t)$$

$$y(t) = [2 \quad 3] \mathbf{x}(t)$$

- Mathematically, the other pole at -2 got canceled because of the 0 in the vector **B** together with **A** being diagonal which basically means that the dynamics of the second state cannot be controlled by the input (the input has not control over x_2) or we say x_2 is not controllable
- If you dig deep, you can discover what happened to the eigenvalue at -2 and why it disappeared in TF
- It is because the system has a zero also at -2 that got canceled with the pole at -2 (How can you check zeros??)

$$\begin{vmatrix} z_0 \mathbf{I} - \mathbf{A} & -\mathbf{B} \\ \mathbf{C} & \mathbf{D} \end{vmatrix} = 0$$

Controllability definition

14

$$\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k)$$

$$\mathbf{x}(k) = \mathbf{A}^k \mathbf{x}(0) + \sum_{j=0}^{k-1} \mathbf{A}^{k-1-j} \mathbf{B}\mathbf{u}(j)$$

Assume zero initial state vector, $\mathbf{x}(0) = 0$ (will get back to remove this assumption later)

$$\mathbf{x}(k) = \sum_{j=0}^{k-1} \mathbf{A}^{k-1-j} \mathbf{B}\mathbf{u}(j)$$

$n \times 1$

$$= \underbrace{\begin{bmatrix} \mathbf{B} & \mathbf{A}\mathbf{B} & \mathbf{A}^2\mathbf{B} & \dots & \mathbf{A}^{k-1}\mathbf{B} \end{bmatrix}}_{\substack{n \times kp \\ \text{Controllability matrix } \mathbf{C}_k}} \begin{bmatrix} \mathbf{u}(k-1) \\ \mathbf{u}(k-2) \\ \mathbf{u}(k-3) \\ \vdots \\ \mathbf{u}(0) \end{bmatrix}$$

$kp \times 1$

Input vector \mathbf{U} is a concatenation of k input vectors each is $p \times 1$

Controllability definition

15

$$\mathbf{x}(k) = \sum_{j=0}^{k-1} \mathbf{A}^{k-1-j} \mathbf{B} \mathbf{u}(j)$$

$n \times 1$

$$= \underbrace{\begin{bmatrix} \mathbf{B} & \mathbf{A}\mathbf{B} & \mathbf{A}^2\mathbf{B} & \dots & \mathbf{A}^{k-1}\mathbf{B} \end{bmatrix}}_{\substack{n \times kp \\ \text{Controllability matrix } \mathbf{C}_k}} \begin{bmatrix} \mathbf{u}(k-1) \\ \mathbf{u}(k-2) \\ \mathbf{u}(k-3) \\ \vdots \\ \mathbf{u}(0) \end{bmatrix}$$

$kp \times 1$

Input vector is a concatenation of k input vectors each is $p \times 1$

$\Rightarrow \mathbf{x}(k) = \mathbf{C}_k \mathbf{U}$

Controllability Definition

- The system is said to be controllable if there exists a succession of inputs that can steer the system from an initial state vector to any desired state vector at time k (Important as will be related to controller design)
- In other words, if there is a solution for \mathbf{U} to get any $\mathbf{x}(k)$ in the above equation (\mathbf{U} exists for any left hand side target $\mathbf{x}(k)$)

Controllability mathematical condition

16

$$\mathbf{x}(k) = \begin{bmatrix} \mathbf{B} & \mathbf{A}\mathbf{B} & \mathbf{A}^2\mathbf{B} & \dots & \mathbf{A}^{k-1}\mathbf{B} \end{bmatrix} \begin{bmatrix} \mathbf{u}(k-1) \\ \mathbf{u}(k-2) \\ \mathbf{u}(k-3) \\ \vdots \\ \mathbf{u}(0) \end{bmatrix} \rightarrow \boxed{\mathbf{x}(k) = \mathbf{C}_k \mathbf{U}}$$

Controllability condition

- For the system to be controllable, \mathbf{C}_k must be full rank, i.e. $\text{rank}(\mathbf{C}_k) = n$ (why?)
- When \mathbf{C}_k is full rank, the range of \mathbf{C}_k or its column space is the whole space \mathbb{R}^n and not just a subspace in it
- Usually \mathbf{C}_k is a fat matrix (columns > rows)
- Need to check if there are n columns of \mathbf{C}_k that are independent or not (pivot columns)
- If they are independent, this means that a linear combination of the columns of \mathbf{C}_k spans the entire \mathbb{R}^n and the system is controllable

Controllability mathematical condition

17

illustrative example

- Check controllability of system whose \mathbf{C}_k is

$$\mathbf{C}_k = \begin{bmatrix} 1 & 2 & 3 \\ 2 & 4 & 6 \end{bmatrix}$$

$\text{rank}\{\mathbf{C}_k\} = 1$ (why?) \rightarrow col.2 is $2 \cdot$ col. 1 and col.3 is $3 \cdot$ col.1

Formal way is to do Gaussian elimination and find the number of pivot columns (to get reduced row echelon form)

$$\begin{aligned} \mathbf{C}_k \mathbf{U} &= \begin{bmatrix} 1 & 2 & 3 \\ 2 & 4 & 6 \end{bmatrix} \begin{bmatrix} u(1) \\ u(2) \\ u(3) \end{bmatrix} \\ &= u(1) \begin{bmatrix} 1 \\ 2 \end{bmatrix} + u(2) \begin{bmatrix} 2 \\ 4 \end{bmatrix} + u(3) \begin{bmatrix} 3 \\ 6 \end{bmatrix} \\ &= (u(1) + 2u(2) + 3u(3)) \begin{bmatrix} 1 \\ 2 \end{bmatrix} \end{aligned}$$


In this case the column space of this rank deficient matrix is a subspace (line) in \mathbf{R}^2

Controllability mathematical condition

18

Note

- When \mathbf{C}_k is fat, i.e. when $k > n$, you do not need to check the rank of \mathbf{C}_k but you can only check the rank of \mathbf{C}_n (why?)

$$\mathbf{C}_k = \left[\mathbf{B} \quad \mathbf{A}\mathbf{B} \quad \mathbf{A}^2\mathbf{B} \quad \dots \quad \mathbf{A}^{n-1}\mathbf{B} \quad \mathbf{A}^n\mathbf{B} \quad \dots \quad \mathbf{A}^{k-1}\mathbf{B} \right]$$


Check only these columns because the rest of the columns will be dependent on them (why?)

- Because from Cayley-Hamilton theorem, every square matrix satisfies its own characteristic equation and hence $\mathbf{A}^n \mathbf{B}$ will depend on previous columns $|\mathbf{A} - \lambda \mathbf{I}| = 0$

$$\lambda^n + a_{n-1}\lambda^{n-1} + a_{n-2}\lambda^{n-2} + \dots + a_1\lambda + a_0 = 0$$

$$\mathbf{A}^n + a_{n-1}\mathbf{A}^{n-1} + a_{n-2}\mathbf{A}^{n-2} + \dots + a_1\mathbf{A} + a_0\mathbf{I} = 0$$

$$\therefore \mathbf{A}^n = -a_{n-1}\mathbf{A}^{n-1} - a_{n-2}\mathbf{A}^{n-2} - \dots - a_1\mathbf{A} + a_0\mathbf{I}$$

Controllability mathematical condition

19

Summary

- A system with matrices \mathbf{A}, \mathbf{B} is said to be controllable if its controllability matrix is full rank (same for continuous and discrete)

$$\text{rank} \{ \mathbf{C}_n \} = n$$

$$\mathbf{C}_n = \begin{bmatrix} \mathbf{B} & \mathbf{A}\mathbf{B} & \mathbf{A}^2\mathbf{B} & \dots & \mathbf{A}^{n-1}\mathbf{B} \end{bmatrix}$$

Final Note

- What if initial state vector is not zero?

$$\mathbf{x}(k) = \mathbf{A}^k \mathbf{x}(0) + \mathbf{C}_k \mathbf{U} \quad \Rightarrow \quad \mathbf{x}(k) - \mathbf{A}^k \mathbf{x}(0) = \mathbf{C}_k \mathbf{U}$$

- Condition of controllability stays the same since going from non-zero $\mathbf{x}(0)$ to $\mathbf{x}(k)$ is just equivalent to going from zero initial state vector to $\mathbf{x}(k) - \mathbf{A}^k \mathbf{x}(0)$

Observability concept

20

Illustrative Example

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 3 \\ 1 \end{bmatrix} u(t)$$

$$y(t) = \begin{bmatrix} 2 & 0 \end{bmatrix} \mathbf{x}(t)$$

- Eigenvalues of \mathbf{A} are -1, -2 (poles of the system)
- Let's find the TF

$$TF = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}$$

$$= \begin{bmatrix} 2 & 0 \end{bmatrix} \begin{bmatrix} \frac{1}{s+1} & 0 \\ 0 & \frac{1}{s+2} \end{bmatrix} \begin{bmatrix} 3 \\ 1 \end{bmatrix}$$

$$= \frac{6}{s+1}$$

Same TF as example in slide 12
Where is the other pole at -2 ?

Observability concept

21

Illustrative Example

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 3 \\ 1 \end{bmatrix} u(t)$$

$$y(t) = \begin{bmatrix} 2 & 0 \end{bmatrix} \mathbf{x}(t)$$

- Mathematically, the other pole at -2 got canceled because of the 0 in **C** together with **A** being diagonal which basically means that the dynamics of the second state cannot be observed at the output or we say x_2 is not observable
- If you dig deep, you can discover what happened to the eigenvalue at -2 and why it disappeared in TF
- It is because the system has a zero also at -2 that got canceled with the pole at -2 (How can you check zeros??)

$$\begin{vmatrix} z_0 \mathbf{I} - \mathbf{A} & -\mathbf{B} \\ \mathbf{C} & \mathbf{D} \end{vmatrix} = 0$$

Observability definition

22

$$\mathbf{x}(k + 1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k)$$

$$\mathbf{x}(k) = \mathbf{A}^k \mathbf{x}(0) + \sum_{j=0}^{k-1} \mathbf{A}^{k-1-j} \mathbf{B}\mathbf{u}(j)$$

Output Equation



$$\mathbf{y}(k) = \mathbf{C}\mathbf{x}(k) + \mathbf{D}\mathbf{u}(k)$$

$$= \mathbf{C}\mathbf{A}^k \mathbf{x}(0) + \sum_{j=0}^{k-1} \mathbf{C}\mathbf{A}^{k-1-j} \mathbf{B}\mathbf{u}(j) + \mathbf{D}\mathbf{u}(k)$$

Observability Definition

- The system is said to be observable if I can uniquely know the initial state variables with the knowledge of the succession of inputs and outputs over finite period of time
- Very important concept as it will be related to State observers that will estimate the state variables from the knowledge of input and output

Observability mathematical condition

23

$$\begin{aligned}\mathbf{y}(k) &= \mathbf{C}\mathbf{x}(k) + \mathbf{D}\mathbf{u}(k) \\ &= \mathbf{C}\mathbf{A}^k \mathbf{x}(0) + \sum_{j=0}^{k-1} \mathbf{C}\mathbf{A}^{k-1-j} \mathbf{B}\mathbf{u}(j) + \mathbf{D}\mathbf{u}(k)\end{aligned}$$

$$\mathbf{y}(0) = \mathbf{C}\mathbf{x}(0) + \mathbf{D}\mathbf{u}(0)$$

$$\mathbf{y}(1) = \mathbf{C}\mathbf{A}\mathbf{x}(0) + \mathbf{C}\mathbf{B}\mathbf{u}(0) + \mathbf{D}\mathbf{u}(1)$$

$$\mathbf{y}(2) = \mathbf{C}\mathbf{A}^2\mathbf{x}(0) + \mathbf{C}\mathbf{A}\mathbf{B}\mathbf{u}(0) + \mathbf{C}\mathbf{B}\mathbf{u}(1) + \mathbf{D}\mathbf{u}(2)$$

⋮ ⋮ ⋮ ⋮ ⋮

Observability mathematical condition

24

$$\mathbf{y}(0) = \mathbf{C}\mathbf{x}(0) + \mathbf{D}\mathbf{u}(0)$$

$$\mathbf{y}(1) = \mathbf{C}\mathbf{A}\mathbf{x}(0) + \mathbf{C}\mathbf{B}\mathbf{u}(0) + \mathbf{D}\mathbf{u}(1)$$

$$\mathbf{y}(2) = \mathbf{C}\mathbf{A}^2\mathbf{x}(0) + \mathbf{C}\mathbf{A}\mathbf{B}\mathbf{u}(0) + \mathbf{C}\mathbf{B}\mathbf{u}(1) + \mathbf{D}\mathbf{u}(2)$$

$$\begin{array}{c} \vdots \\ \vdots \\ \vdots \\ \vdots \\ \vdots \end{array}$$

$$\begin{bmatrix} \mathbf{y}(0) \\ \mathbf{y}(1) \\ \mathbf{y}(2) \\ \vdots \\ \mathbf{y}(k-1) \end{bmatrix} = \begin{bmatrix} \mathbf{C} \\ \mathbf{C}\mathbf{A} \\ \mathbf{C}\mathbf{A}^2 \\ \vdots \\ \mathbf{C}\mathbf{A}^{k-1} \end{bmatrix} \mathbf{x}(0) + \begin{bmatrix} \mathbf{D} & 0 & 0 & 0 & \dots & 0 \\ \mathbf{C}\mathbf{B} & \mathbf{D} & 0 & 0 & \dots & 0 \\ \mathbf{C}\mathbf{A}\mathbf{B} & \mathbf{C}\mathbf{B} & \mathbf{D} & 0 & \dots & 0 \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ \mathbf{C}\mathbf{A}^{k-2}\mathbf{B} & \mathbf{C}\mathbf{A}^{k-3}\mathbf{B} & \dots & \mathbf{C}\mathbf{A}\mathbf{B} & \mathbf{C}\mathbf{B} & \mathbf{D} \end{bmatrix} \begin{bmatrix} \mathbf{u}(0) \\ \mathbf{u}(1) \\ \mathbf{u}(2) \\ \vdots \\ \mathbf{u}(k-1) \end{bmatrix}$$

$mk \times 1$
 $mk \times n$
 $mk \times pk$
 $pk \times 1$

$$\mathbf{Y} = \mathbf{O}_k \mathbf{x}(0) + \mathbf{V}_k \mathbf{U}$$

Observability mathematical condition

25

$$\mathbf{Y} = \mathbf{O}_k \mathbf{x}(0) + \mathbf{V}_k \mathbf{U}$$

$$\mathbf{O}_k \mathbf{x}(0) = \mathbf{Y} - \mathbf{V}_k \mathbf{U}$$

- If I know the inputs and outputs, I know the right hand side of the above equation
- $\mathbf{x}(0)$ is uniquely defined only if $\text{rank}\{\mathbf{O}_k\} = n$ (Why?)
- If \mathbf{O}_k is rank deficient then its nullspace is not empty \rightarrow say $\mathbf{v} \in N(\mathbf{O}_k)$

$$\mathbf{O}_k \mathbf{x}(0) = \mathbf{O}_k [\mathbf{x}(0) + \mathbf{v}] = \mathbf{Y} - \mathbf{V}_k \mathbf{U}$$

- If \mathbf{O}_k is a full rank matrix, its nullspace is empty other than zero vector hence if LHS is known, $\mathbf{x}(0)$ is uniquely determined
- Usually \mathbf{O}_k is a tall matrix

Observability mathematical condition

26

Summary

- A system with matrices \mathbf{A}, \mathbf{C} is said to be observable if its observability matrix is full rank (check only rank of \mathbf{O}_n if $k > n$)

$$\text{rank} \{ \mathbf{O}_n \} = n$$
$$\mathbf{O}_n = \begin{bmatrix} \mathbf{C} \\ \mathbf{CA} \\ \mathbf{CA}^2 \\ \vdots \\ \mathbf{CA}^{n-1} \end{bmatrix}$$

Minimal realization

27

Illustrative Example

$$\dot{\mathbf{x}}(t) = -2\mathbf{x}(t) + 3u(t)$$

$$y(t) = 2\mathbf{x}(t)$$

$$TF = \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}$$

$$= 2 \cdot \frac{1}{s+2} \cdot 3$$

$$= \frac{6}{s+1}$$

Same TF as example in
slides 12 and 20

- Both previous examples led to the same TF but one was uncontrollable and the second was unobservable
- This realization of the same TF is both controllable and observable because it is the **minimal realization** (only 1 state variable not 2)

A minimal realization is both controllable and observable (without proof)