

State Feedback and State Estimators

“Linear System Theory and Design”, Chapter 8

<http://zitompul.wordpress.com>

2014

A state-space equation of a third-order system is given as:

$$\dot{\underline{\tilde{\mathbf{x}}}}(t) = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -2 & 0 \\ 0 & 0 & -3 \end{bmatrix} \underline{\tilde{\mathbf{x}}}(t) + \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} u(t)$$

$$y(t) = [6 \quad -6 \quad 1] \underline{\tilde{\mathbf{x}}}(t)$$

- Perform a step-by-step transformation of the given model to Frobenius Form.
- Calculate the required feedback gain $\underline{\mathbf{k}}$ so that the system may have two conjugate poles at $-2 \pm j1$ and -4 .

Solution of Homework 5

a. Transformation to Frobenius Form.

- Find the characteristic equation $a(s) = \det(s\underline{\mathbf{I}} - \underline{\mathbf{A}}) = \det \left(\begin{bmatrix} s+1 & 0 & 0 \\ 0 & s+2 & 0 \\ 0 & 0 & s+3 \end{bmatrix} \right)$

$$= (s+1)(s+2)(s+3)$$

$$= s^3 + 6s^2 + 11s + 6$$

- Calculate $\underline{\mathcal{C}}, \underline{\mathcal{J}}$

$$\underline{\mathcal{C}} = [\underline{\mathbf{b}} \quad \underline{\mathbf{A}}\underline{\mathbf{b}} \quad \underline{\mathbf{A}}^2\underline{\mathbf{b}}] = \begin{bmatrix} 1 & -1 & 1 \\ 1 & -2 & 4 \\ 1 & -3 & 9 \end{bmatrix}$$

$$\underline{\mathcal{J}} = \begin{bmatrix} a_1 & a_2 & 1 \\ a_2 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 11 & 6 & 1 \\ 6 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix}$$

Solution of Homework 5

• Calculate $\underline{\mathbf{Q}}$

$$\underline{\mathbf{Q}} = \underline{\mathbf{e}}\underline{\mathbf{f}} = \begin{bmatrix} 1 & -1 & 1 \\ 1 & -2 & 4 \\ 1 & -3 & 9 \end{bmatrix} \begin{bmatrix} 11 & 6 & 1 \\ 6 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 6 & 5 & 1 \\ 3 & 4 & 1 \\ 2 & 3 & 1 \end{bmatrix}$$

$$\underline{\mathbf{Q}}^{-1} = \begin{bmatrix} 0.5 & -1 & 0.5 \\ -0.5 & 2 & -1.5 \\ 0.5 & -4 & 4.5 \end{bmatrix}$$

• Perform transformation

$$\underline{\hat{\mathbf{A}}} = \underline{\mathbf{Q}}^{-1} \underline{\mathbf{A}} \underline{\mathbf{Q}} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -6 & -11 & -6 \end{bmatrix}$$

$$\underline{\hat{\mathbf{b}}} = \underline{\mathbf{Q}}^{-1} \underline{\mathbf{b}} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$

• Transformation accomplished

Solution of Homework 5

b. Finding \underline{k} .

- Calculate $\hat{\underline{k}}$

$$\bar{a}(s) = (s + 2 - j) \cdot (s + 2 + j) \cdot (s + 4)$$

$$\bar{a}(s) = s^3 + 8s^2 + 21s + 20$$

$$a(s) = s^3 + 6s^2 + 11s + 6$$

$$\left. \begin{aligned} \hat{k}_1 &= \bar{a}_0 - a_0 = 14 \\ \hat{k}_2 &= \bar{a}_1 - a_1 = 10 \\ \hat{k}_3 &= \bar{a}_2 - a_2 = 2 \end{aligned} \right\} \hat{\underline{k}} = [14 \quad 10 \quad 2]$$

- Calculate \underline{k}

$$\underline{k} = \hat{\underline{k}} \underline{Q}^{-1}$$

$$= [14 \quad 10 \quad 2] \begin{bmatrix} 0.5 & -1 & 0.5 \\ -0.5 & 2 & -1.5 \\ 0.5 & -4 & 4.5 \end{bmatrix}$$

$$= \underline{\underline{[3 \quad -2 \quad 1]}}$$

Solution of Homework 5

c. Direct calculation of $\underline{\mathbf{k}}$ without transformation.

$$a(s) = \det(s\underline{\mathbf{I}} - (\underline{\mathbf{A}} - \underline{\mathbf{b}}\underline{\mathbf{k}}))$$

$$= \det \left(s \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} - \left(\begin{bmatrix} -1 & 0 & 0 \\ 0 & -2 & 0 \\ 0 & 0 & -3 \end{bmatrix} - \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} \begin{bmatrix} k_1 & k_2 & k_3 \end{bmatrix} \right) \right)$$

$$= \det \left(s \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} - \begin{bmatrix} -(1+k_1) & -k_2 & -k_3 \\ -k_1 & -(2+k_2) & -k_3 \\ -k_1 & -k_2 & -(3+k_3) \end{bmatrix} \right)$$

$$= \det \left(\begin{bmatrix} s + (1+k_1) & k_2 & k_3 \\ k_1 & s + (2+k_2) & k_3 \\ k_1 & k_2 & s + (3+k_3) \end{bmatrix} \right)$$

• **Complicated to be done**

Output Feedback

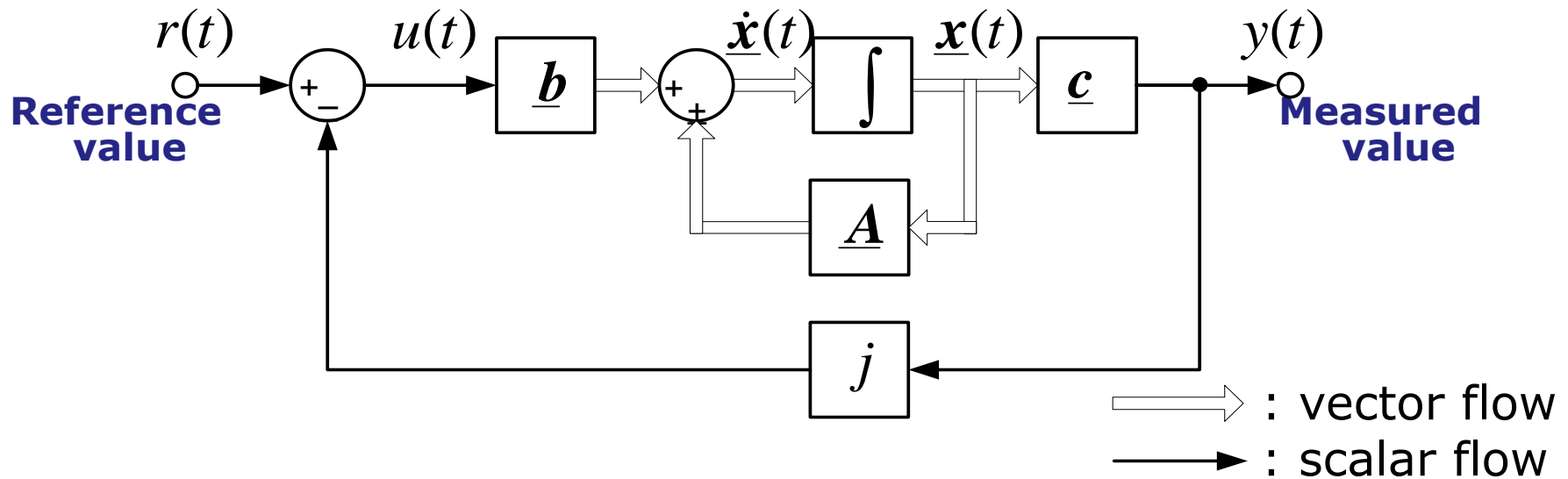
- Consider the n -dimensional **controllable** single-variable state space equations:

$$\dot{\underline{x}}(t) = \underline{A}\underline{x}(t) + \underline{b}u(t)$$

$$y(t) = \underline{c}\underline{x}(t)$$

- **Main idea:** Using measurement of output variable $y(t)$, determine an input $u(t)=f(r(t),y(t))$ such that the dynamic properties of the system can be changed to fulfill a certain criteria.
- In contrast to state feedback, output feedback has less degree of freedom in the controller parameter.
- However, the output feedback method is superior to the state feedback method from the practical point of view, because the output $y(t)$ is known and measurable.
- On the contrary, it is almost always difficult, if not impossible, to measure the entire state vector $x(t)$ due to practical limitations. (This can be encompassed by using state observer which will be discussed later.)

Output Feedback



- The output $y(t)$ is fed back through a feedback gain j .
- The input $u(t)$ is given by:

$$\begin{aligned}
 u(t) &= r(t) - jy(t) \\
 &= r(t) - j\underline{c}\underline{x}(t)
 \end{aligned}$$

- By inspection the state feedback gain \underline{k} and output feedback gain j are actually related via the following equation:

$$\underline{k} \Leftrightarrow j\underline{c}$$

Output Feedback

- Substituting $u(t)$ to the original state space equations,

$$\dot{\underline{x}}(t) = (\underline{A} - j\underline{b}\underline{c})\underline{x}(t) + \underline{b}r(t)$$

$$y(t) = \underline{c}\underline{x}(t)$$

- The roots of the characteristic equation can now be repositioned through

$$a(s) = \det(s\underline{I} - (\underline{A} - j\underline{b}\underline{c}))$$

- The output feedback has less degree of freedom in placing the poles, thus it may happen that the location to place the poles is limited.

Example: Output Feedback

Let us redo the previous example with the following state equations:

$$\underline{\dot{\mathbf{x}}}(t) = \begin{bmatrix} 1 & 3 \\ 3 & 1 \end{bmatrix} \underline{\mathbf{x}}(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$

$$y(t) = [1 \quad 1] \underline{\mathbf{x}}(t)$$

The characteristic equation of the given system is:

$$\begin{aligned} a(s) &= \det(s\mathbf{I} - \mathbf{A}) \\ &= (s - 4)(s + 2) \end{aligned} \bullet \text{ **Unstable eigenvalues** } \\ &\quad \text{or **unstable pole**}$$

Introducing the output feedback,

$$u(t) = r(t) - jy(t) = r(t) - j\underline{\mathbf{b}}\underline{\mathbf{c}}\underline{\mathbf{x}}(t)$$

The state space is now:

$$\underline{\dot{\mathbf{x}}}(t) = \begin{bmatrix} 1 & 3 \\ 3 - j & 1 - j \end{bmatrix} \underline{\mathbf{x}}(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} r(t)$$

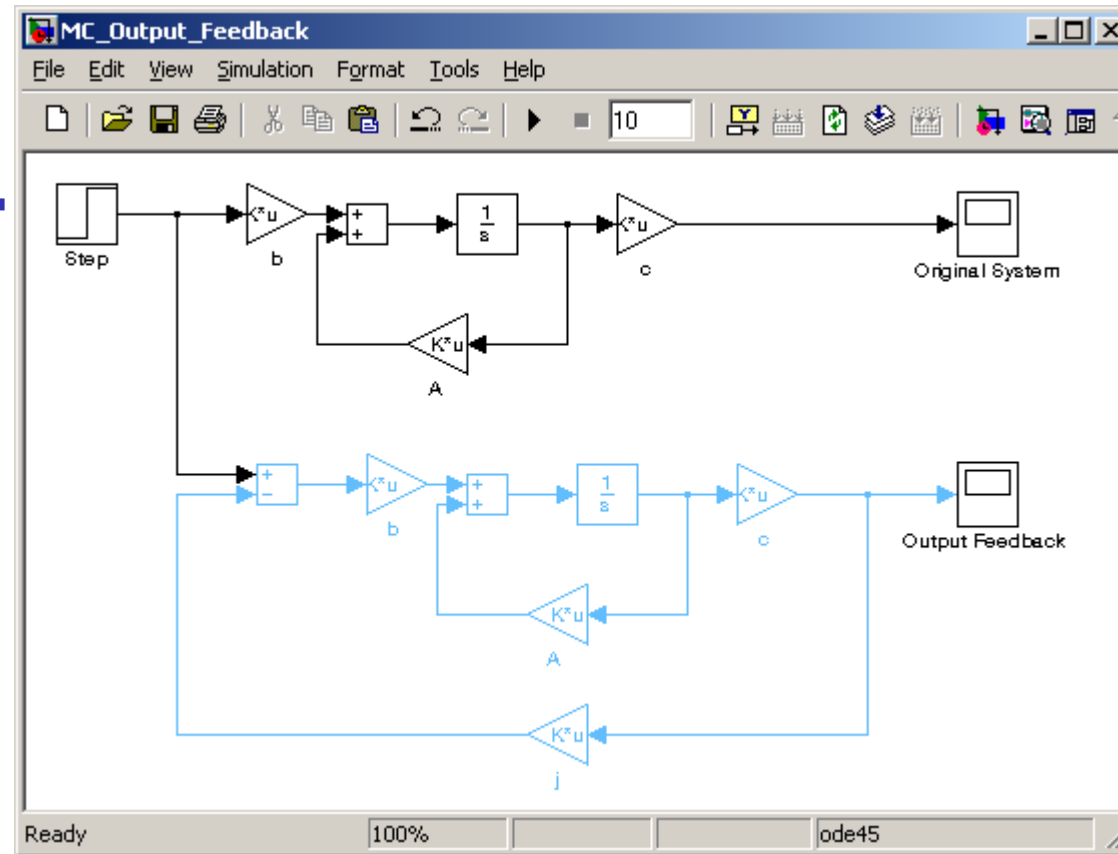
Example: Output Feedback

The characteristic equation becomes:

$$\begin{aligned} a(s) &= \det \left(\begin{bmatrix} s-1 & -3 \\ -(3-j) & s-(1-j) \end{bmatrix} \right) \\ &= (s-1)(s-(1-j)) - (3-j)(3) \\ &= s^2 + \underbrace{(j-2)}_{} s + \underbrace{(2j-8)}_{} \end{aligned}$$

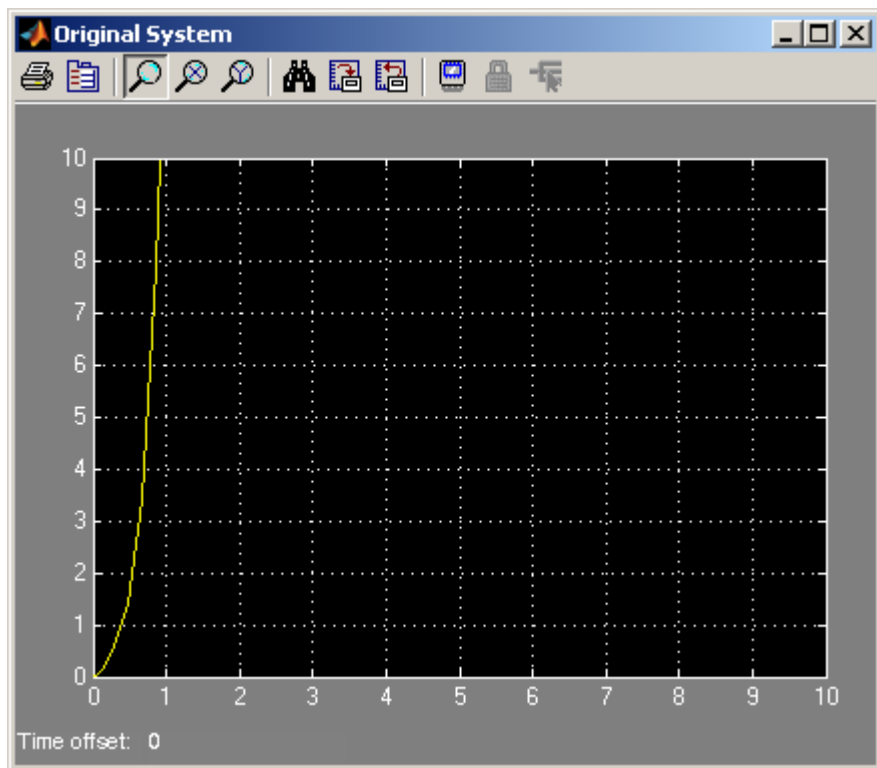
- **The roots of the new characteristic equation can be moved to a new stable position.**
- **But, the value of the stable poles cannot be freely chosen.**

Example: Output Feedback

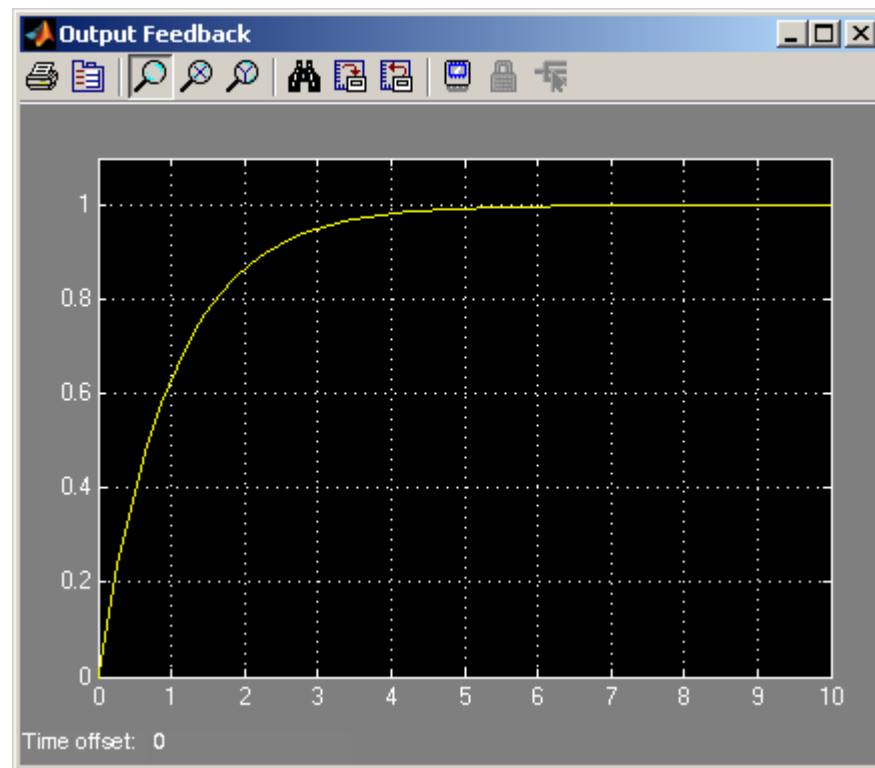


- Matlab Simulink realization

Example: Output Feedback



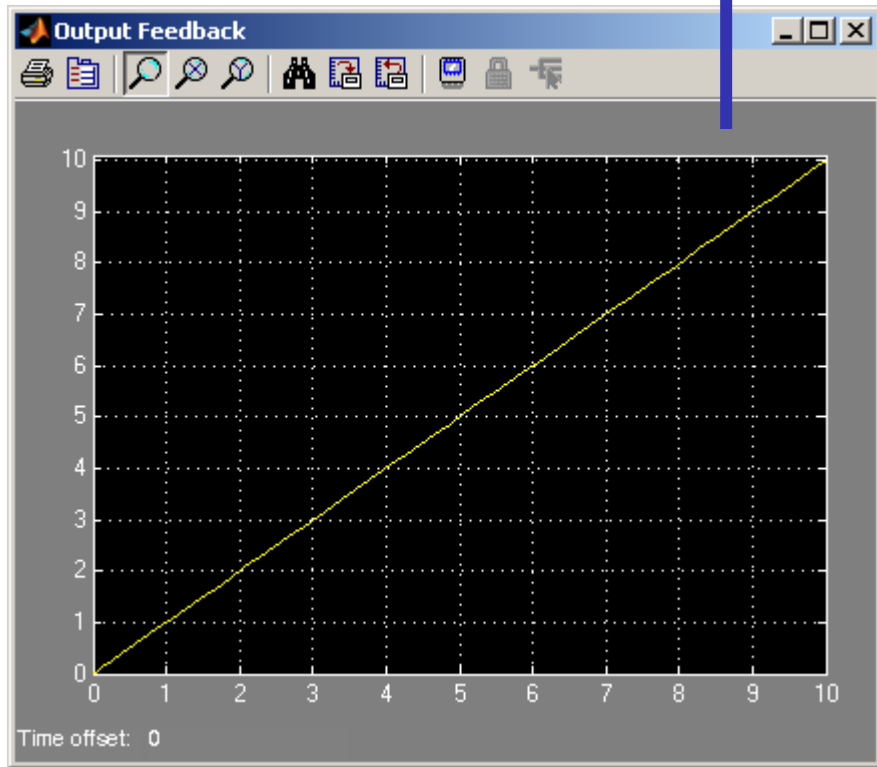
- Output of original system



- Output of system with output feedback, $j = 5$

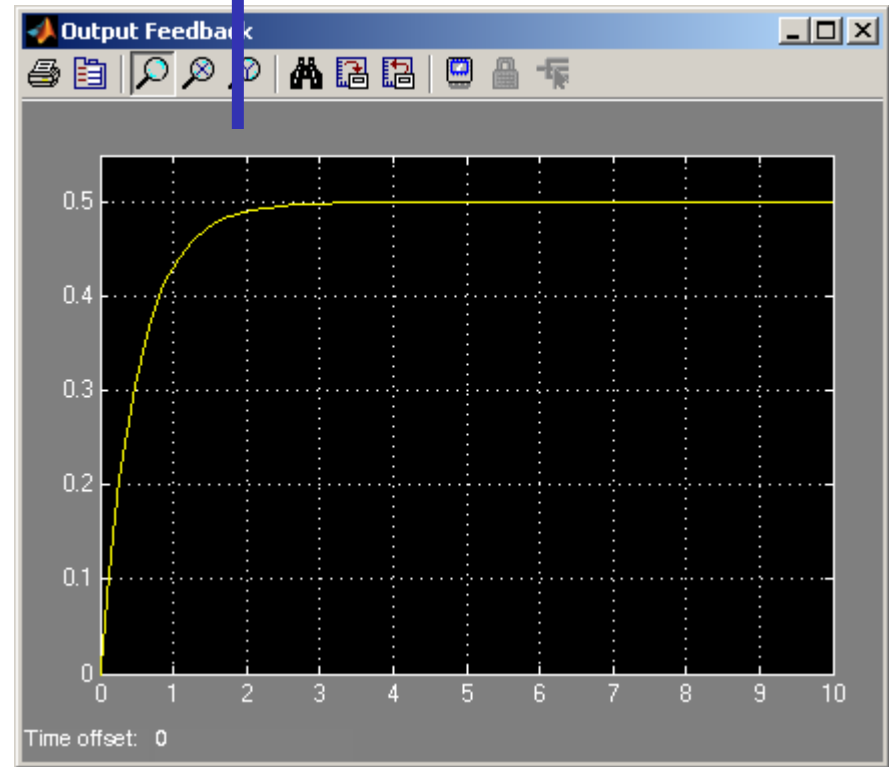
Example: Output Feedback

One pole at the origin,
Integrator property



- Output of system with output feedback, $j = 4$

Steady-state error



- Output of system with output feedback, $j = 6$