Semiconductor Device Physics

Lecture 7

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Semiconductor Device Physics

Chapter 6 *pn* **Junction Diodes:** *I***-***V* **Characteristics**

Qualitative Derivation

Current Flow in a *pn* Junction Diode

- When a forward bias (V_A > 0) is applied, the potential barrier to diffusion across the junction is reduced.
- Minority carriers are "injected" into the quasi-neutral regions $\rightarrow \Delta n_{\rm o} > 0$, $\Delta p_{\rm o} > 0$.
- **Minority carriers diffuse in the quasi-neutral regions,** recombining with majority carriers.

Ideal Diode: Assumptions

- Steady-state conditions.
- Non-degenerately doped step junction.
- ■One-dimensional diode.
- **Low-level injection conditions prevail in the quasi-neutral** regions.
- No processes other than drift, diffusion, and thermal R–G take place inside the diode.

Current Flow in a *pn* Junction Diode

 \blacksquare Current density $J = J_N(x) + J_P(x)$

$$
\mathbf{J}_{N}(x) = q\mu_{n}n\mathbf{\mathcal{E}} + qD_{N}\frac{dn}{dx} = q\mu_{n}n\mathbf{\mathcal{E}} + qD_{N}\frac{d(\Delta n)}{dx}
$$

$$
\mathbf{J}_{P}(x) = q\mu_{p}p\mathbf{\mathcal{E}} - qD_{P}\frac{dp}{dx} = q\mu_{p}p\mathbf{\mathcal{E}} - qD_{P}\frac{d(\Delta p)}{dx}
$$

- \blacksquare **J**_N(*x*) and **J**_P(*x*) may vary with position, but **J** is constant throughout the diode.
- Yet an additional assumption is now made, that thermal recombination-generation is negligible throughout the depletion region \rightarrow J_N and J_P are therefore determined to be constants independent of position inside the depletion region.

Carrier Concentrations at $-x_p$, $+x_n$

Consider the **equilibrium** carrier concentrations at $V_A = 0$:

If low-level injection conditions prevail in the quasi-neutral regions when $V_{\rm A} \neq 0$, then:

$$
p_{p}(-x_{p}) = N_{A}
$$
 $n_{n}(x_{n}) = N_{D}$

"Law of the Junction"

- The voltage *V*_A applied to a *pn* junction **falls mostly across the depletion region** (assuming that low-level injection conditions prevail in the quasi-neutral regions).
- **Two quasi-Fermi levels is drawn in the depletion region:**

$$
p = n_{\mathrm{i}}e^{(E_{\mathrm{i}}-F_{\mathrm{p}})/kT}
$$

$$
n = n_{\mathrm{i}}e^{(F_{\mathrm{N}}-E_{\mathrm{i}})/kT}
$$

$$
np = n_{i}^{2} e^{(E_{i} - F_{P})/kT} e^{(F_{N} - E_{i})/kT}
$$

$$
= n_{i}^{2} e^{(F_{N} - F_{P})/kT}
$$

$$
np = n_{\rm i}^2 e^{qV_{\rm A}/kT}
$$

for $-x_{\text{n}} \leq x \leq x_{\text{n}}$

Excess Carrier Concentrations at $-x_p$, x_n

*p***-side** *n***-side**

$$
p_{p}(-x_{p}) = N_{A}
$$

$$
n_{p}(-x_{p}) = \frac{n_{i}^{2} e^{qV_{A}/kT}}{N_{A}}
$$

$$
= n_{p0} e^{qV_{A}/kT}
$$

$$
\Delta n_{\rm p}(-x_{\rm p}) = \frac{n_{\rm i}^2}{N_{\rm A}} (e^{qV_{\rm A}/kT} - 1) \qquad \Delta p_{\rm n}(x_{\rm n}) = \frac{n_{\rm i}^2}{N_{\rm D}} (e^{qV_{\rm A}}
$$

$$
n_{n}(x_{n}) = N_{D}
$$

$$
p_{n}(x_{n}) = \frac{n_{i}^{2} e^{qV_{A}/kT}}{N_{D}}
$$

$$
= p_{n0} e^{qV_{A}/kT}
$$

$$
\Delta p_{n}(x_{n}) = \frac{n_{i}^{2}}{N_{D}}(e^{qV_{A}/kT} - 1)
$$

Example: Carrier Injection

■ A *pn* junction has N_A =10¹⁸ cm⁻³ and N_D =10¹⁶ cm⁻³. The applied voltage is 0.6 V.

a) What are the minority carrier concentrations at the depletion-region edges?

$$
n_{\rm p}(-x_{\rm p}) = n_{\rm p0}e^{qV_{\rm A}/kT} = 100 \times e^{0.6/0.02586} = \underbrace{1.192 \times 10^{12} \text{ cm}^{-3}}_{= 1.192 \times 10^{14} \text{ cm}^{-3}}
$$

$$
p_{\rm n}(x_{\rm n}) = p_{\rm n0}e^{qV_{\rm A}/kT} = 10^4 \times e^{0.6/0.02586} = \underbrace{1.192 \times 10^{14} \text{ cm}^{-3}}_{= 1.192 \times 10^{14} \text{ cm}^{-3}}
$$

b) What are the excess minority carrier concentrations?

b) What are the excess minority carrier concentrations?
\n
$$
\Delta n_{\text{p}}(-x_{\text{p}}) = n_{\text{p}}(-x_{\text{p}}) - n_{\text{p0}} = 1.192 \times 10^{12} - 100 = 1.192 \times 10^{12} \text{ cm}^{-3}
$$
\n
$$
\Delta p_{\text{n}}(x_{\text{n}}) = p_{\text{n}}(x_{\text{n}}) - p_{\text{n0}} = 1.192 \times 10^{14} - 10^{4} = 1.192 \times 10^{14} \text{ cm}^{-3}
$$

Excess Carrier Distribution

Figure From the minority carrier diffusion equation,

$$
0 = D_{\rm p} \frac{d^2 \Delta p_{\rm n}}{dx^2} - \frac{\Delta p_{\rm n}}{\tau_{\rm p}}, \quad x' \ge 0
$$

■ We have the following boundary conditions:

$$
\Delta p_{n}(x_{n}) = p_{n0}(e^{qV_{A}/kT} - 1)
$$

$$
\Delta p_{n}(\infty) \to 0
$$

For simplicity, we develop a new coordinate system:

for $x' \geq 0$ **Then, the solution is given** by:

$$
\Delta p_{n}(x') = A_{1}e^{-x'/L_{P}} + A_{2}e^{x'/L_{P}}
$$

$$
L_{\rm P}=\sqrt{D_{\rm P}\tau_{\rm p}}
$$

• *L***^P : hole minority carrier diffusion length**

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Excess Carrier Distribution

$$
\Delta p_{n}(x') = A_{1}e^{-x/L_{P}} + A_{2}e^{x/L_{P}}
$$

New boundary conditions

$$
\Delta p_{n}(x' \to 0) = p_{n0}(e^{qV_{A}/kT} - 1)
$$

$$
\Delta p_{n}(x' \to \infty) = 0
$$

From the
$$
x' \rightarrow \infty
$$
, $A_2 = 0$
\n**From the** $x' \rightarrow 0$, $A_1 = p_{n0} (e^{qV_A/kT} - 1)$

Therefore

$$
\Delta p_{n}(x') = p_{n0}(e^{qV_{A}/kT} - 1)e^{-x'/L_{P}}, \quad x' \ge 0
$$

Similarly,

$$
\Delta n_{\rm p}(x'') = n_{\rm p0}(e^{qV_{\rm A}/kT} - 1)e^{-x''/L_{\rm N}}, \quad x'' \ge 0
$$

pn Diode *I–V* Characteristic

n-side
$$
J_{P}(x') = -qD_{P} \frac{d \Delta p_{n}(x')}{dx'} = q \frac{D_{P}}{L_{P}} p_{n0} (e^{qV_{A}/kT} - 1) e^{-x'/L_{P}}
$$

p-side
$$
J_N(x'') = -qD_N \frac{d\Delta n_p(x'')}{dx''} = q\frac{D_N}{L_N} n_{p0} (e^{qV_A/kT} - 1)e^{-x''/L_N}
$$

$$
\mathbf{J} = \mathbf{J}_N \big|_{x = -x_p} + \mathbf{J}_P \big|_{x = x_n} = \mathbf{J}_N \big|_{x' = 0} + \mathbf{J}_P \big|_{x' = 0}
$$

$$
\mathbf{J} = q n_{i}^{2} \left(\frac{D_{N}}{L_{N} N_{A}} + \frac{D_{P}}{L_{P} N_{D}} \right) (e^{q V_{A}/kT} - 1)
$$

pn Diode *I–V* Characteristic

$$
I = A\mathbf{J} = A q n_{i}^{2} \left(\frac{D_{N}}{L_{N} N_{A}} + \frac{D_{P}}{L_{P} N_{D}} \right) (e^{q V_{A}/kT} - 1)
$$

$$
I = A\mathbf{J} = Aqn_i^2 \left(\frac{D_{\rm N}}{L_{\rm N}N_{\rm A}} + \frac{D_{\rm P}}{L_{\rm P}N_{\rm D}} \right)
$$

$$
I = I_0(e^{qV_{\rm A}/kT} - 1)
$$

$$
I_0 = Aqn_i^2 \left(\frac{D_{\rm N}}{L_{\rm N}N_{\rm A}} + \frac{D_{\rm P}}{L_{\rm P}N_{\rm D}} \right)
$$

- **Shockley Equation, for ideal diode**
- *I***⁰ can be viewed as the drift current due to minority carriers generated within the diffusion lengths of the depletion region**

Diode Saturation Current I_0

$$
I_0 = A q n_{\rm i}^2 \left(\frac{D_{\rm P}}{L_{\rm P} N_{\rm D}} + \frac{D_{\rm N}}{L_{\rm N} N_{\rm A}} \right)
$$

I₀ can vary by orders of magnitude, depending on the semiconductor material, due to n_i^2 factor.

If In an asymmetrically doped *pn* junction, the term associated with the more heavily doped side is negligible.

If the *p* side is much more heavily doped,

$$
I_0 \cong A q n_i^2 \left(\frac{D_{\rm P}}{L_{\rm P} N_{\rm D}}\right)
$$

If the *n* side is much more heavily doped,

$$
I_0 \cong A q n_{\rm i}^2 \left(\frac{D_{\rm N}}{L_{\rm N} N_{\rm A}} \right)
$$

Diode Carrier Currents

Carrier Concentration: Forward Bias

Carrier Concentration: Reverse Bias

Deficit of minority carriers near the depletion region.

Depletion region acts like a "sink", draining carriers from the adjacent quasineutral regions

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Breakdown Voltage, V_{BR}

If the reverse bias voltage $(-V_A)$ is so large that the peak electric field exceeds a critical value \mathcal{E}_{CR} , then the junction will "break down" and large reverse current will flow.

$$
\mathcal{E}_{CR} = \sqrt{\frac{2q}{\varepsilon_{\rm S}} \left(\frac{N_{\rm A} N_{\rm D}}{N_{\rm A} + N_{\rm D}} \right)} (V_{\rm bi} + V_{\rm BR}) \cdot
$$
 At breakdown, $V_{\rm A} = -V_{\rm BR}$

Thus, the reverse bias at which breakdown occurs is

$$
V_{\text{BR}} = \frac{\varepsilon_{\text{S}} \varepsilon_{\text{CR}}^2}{2q} \left(\frac{N_{\text{A}} + N_{\text{D}}}{N_{\text{A}} N_{\text{D}}} \right) - V_{\text{bi}}
$$

Breakdown Mechanism: Avalanching

Breakdown Mechanism: Zener Process

Barrier must be thin \rightarrow **dominant** breakdown mechanism when both junction sides are heavily doped.

Potential energy

barrier

Typically, Zener process dominates when V_{BR} < 4.5V in Si at 300K and $N > 10^{18}$ cm⁻³.

Semiconductor Device Physics

Chapter 7 *pn* **Junction Diodes: Small-Signal Admittance**

Small-Signal Diode Biasing

- When reversed-biased, a *pn* junction diode becomes functionally equivalent to a capacitor, whose capacitance decreases as the reverse bias increases.
- Biasing additional a.c. signal v_a can be viewed as a small oscillation of the depletion width about the steady state value.

Chapter 7 *pn* **Junction Diodes: Small-Signal Admittance**

Total *pn* Junction Capacitance

$$
C_{\text{J}} = A \frac{\varepsilon_{\text{s}}}{W}
$$

Minority
carrier
lifetime
$$
C_{\text{D}} = \frac{\tau I_{\text{DC}}}{kT/q}
$$

Junction / depletion capacitance, due to variation of depletion charges

Diffusion capacitance,

due to variation of stored minority charges in the quasineutral regions

- *C***^J dominates at low forward biases, reverse biases.**
- C_{D} dominates at moderate to high forward biases.

Relation Between C_I and V_A

For asymmetrical step junction,

$$
W = \sqrt{\frac{2\mathcal{E}_{\rm s}}{qN_{\rm B}}(V_{\rm bi} - V_{\rm A})}
$$

*N***^B : bulk semiconductor doping,** N_A or N_D as appropriate.

Therefore,

$$
\frac{1}{C_{\rm J}^2} = \frac{W^2}{A^2 \varepsilon_{\rm s}^2} \approx \frac{2}{qN_{\rm B}\varepsilon_{\rm S}A^2}(V_{\rm bi} - V_{\rm A})
$$

- A plot of $1/C_J^2$ versus V_A is linear.
- The slope is inversely proportional to N_{B} .
- An extrapolated $1/C_J^2 = 0$ intercept is equal to V_{bi} .