# **Semiconductor Device Physics**

Lecture 7

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**Semiconductor Device Physics** 

# **Chapter 6** *pn* Junction Diodes: *I-V* Characteristics

#### **Qualitative Derivation**

 $\mathcal{E}_{c}$ 

E<sub>Fn</sub>

E,

Ev

VA



#### Current Flow in a pn Junction Diode

When a forward bias ( $V_A > 0$ ) is applied, the potential barrier to diffusion across the junction is reduced.

■ Minority carriers are "injected" into the quasi-neutral regions →  $\Delta n_p > 0$ ,  $\Delta p_n > 0$ .

Minority carriers diffuse in the quasi-neutral regions, recombining with majority carriers.



### Ideal Diode: Assumptions

- Steady-state conditions.
- Non-degenerately doped step junction.
- One-dimensional diode.
- Low-level injection conditions prevail in the quasi-neutral regions.
- No processes other than drift, diffusion, and thermal R–G take place inside the diode.



#### Current Flow in a *pn* Junction Diode

Current density  $\mathbf{J} = \mathbf{J}_{N}(x) + \mathbf{J}_{P}(x)$ 

$$\mathbf{J}_{\mathrm{N}}(x) = q\mu_{\mathrm{n}}n\mathbf{\mathcal{E}} + qD_{\mathrm{N}}\frac{dn}{dx} = q\mu_{\mathrm{n}}n\mathbf{\mathcal{E}} + qD_{\mathrm{N}}\frac{d(\Delta n)}{dx}$$
$$\mathbf{J}_{\mathrm{P}}(x) = q\mu_{\mathrm{p}}p\mathbf{\mathcal{E}} - qD_{\mathrm{P}}\frac{dp}{dx} = q\mu_{\mathrm{p}}p\mathbf{\mathcal{E}} - qD_{\mathrm{P}}\frac{d(\Delta p)}{dx}$$

- **J**<sub>N</sub>(x) and **J**<sub>P</sub>(x) may vary with position, but **J** is constant throughout the diode.
- Yet an additional assumption is now made, that thermal recombination-generation is negligible throughout the depletion region  $\rightarrow J_N$  and  $J_P$  are therefore determined to be constants independent of position inside the depletion region.

#### Carrier Concentrations at $-x_{\rm p}$ , $+x_{\rm n}$

Consider the **equilibrium** carrier concentrations at  $V_A = 0$ :

<u><i>p</i>-side</u>	<u><i>n</i>-side</u>
$p_{\rm p0}(-x_{\rm p}) = N_{\rm A}$	$n_{\rm n0}(x_{\rm n}) = N_{\rm D}$
$n_{\rm p0}(-x_{\rm p}) = \frac{n_{\rm i}^2}{N_{\rm A}}$	$p_{\rm n0}(x_{\rm n}) = \frac{n_{\rm i}^2}{N_{\rm D}}$

If low-level injection conditions prevail in the quasi-neutral regions when  $V_A \neq 0$ , then:

$$p_{\rm p}(-x_{\rm p}) = N_{\rm A} \qquad n_{\rm n}(x_{\rm n}) = N_{\rm D}$$

#### "Law of the Junction"

- The voltage V<sub>A</sub> applied to a pn junction falls mostly across the depletion region (assuming that low-level injection conditions prevail in the quasi-neutral regions).
- Two quasi-Fermi levels is drawn in the depletion region:



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# Excess Carrier Concentrations at $-x_p$ , $x_n$

#### <u>p-side</u>

$$p_{p}(-x_{p}) = N_{A}$$

$$n_{p}(-x_{p}) = \frac{n_{i}^{2}e^{qV_{A}/kT}}{N_{A}}$$

$$= n_{p0}e^{qV_{A}/kT}$$

$$\Delta n_{\rm p}(-x_{\rm p}) = \frac{n_{\rm i}^2}{N_{\rm A}} (e^{qV_{\rm A}/kT} - 1)$$

#### <u>*n*-side</u>

$$n_{\rm n}(x_{\rm n}) = N_{\rm D}$$

$$p_{\rm n}(x_{\rm n}) = \frac{n_{\rm i}^2 e^{qV_{\rm A}/kT}}{N_{\rm D}}$$

$$= p_{\rm n0} e^{qV_{\rm A}/kT}$$

$$\Delta p_{\rm n}(x_{\rm n}) = \frac{n_{\rm i}^2}{N_{\rm D}} (e^{qV_{\rm A}/kT} - 1)$$

#### **Example:** Carrier Injection

A pn junction has N<sub>A</sub>=10<sup>18</sup> cm<sup>-3</sup> and N<sub>D</sub>=10<sup>16</sup> cm<sup>-3</sup>. The applied voltage is 0.6 V.

a) What are the minority carrier concentrations at the depletion-region edges?

$$n_{\rm p}(-x_{\rm p}) = n_{\rm p0}e^{qV_{\rm A}/kT} = 100 \times e^{0.6/0.02586} = \underline{1.192 \times 10^{12} \text{ cm}^{-3}}$$
$$p_{\rm n}(x_{\rm n}) = p_{\rm n0}e^{qV_{\rm A}/kT} = 10^4 \times e^{0.6/0.02586} = \underline{1.192 \times 10^{14} \text{ cm}^{-3}}$$

b) What are the excess minority carrier concentrations?

$$\Delta n_{\rm p}(-x_{\rm p}) = n_{\rm p}(-x_{\rm p}) - n_{\rm p0} = 1.192 \times 10^{12} - 100 = \underline{1.192 \times 10^{12} \text{ cm}^{-3}}$$
$$\Delta p_{\rm n}(x_{\rm n}) = p_{\rm n}(x_{\rm n}) - p_{\rm n0} = 1.192 \times 10^{14} - 10^{4} = \underline{1.192 \times 10^{14} \text{ cm}^{-3}}$$

### **Excess Carrier Distribution**

From the minority carrier diffusion equation,

$$0 = D_{\rm P} \frac{d^2 \Delta p_{\rm n}}{dx'^2} - \frac{\Delta p_{\rm n}}{\tau_{\rm p}}, \quad x' \ge 0$$

We have the following boundary conditions:

$$\Delta p_{\rm n}(x_{\rm n}) = p_{\rm n0}(e^{qV_{\rm A}/kT} - 1)$$
$$\Delta p_{\rm n}(\infty) \to 0$$

For simplicity, we develop a new coordinate system:



Then, the solution is given by: for  $x' \ge 0$ 

$$\Delta p_{\rm n}(x') = A_{\rm l} e^{-x'/L_{\rm P}} + A_{\rm 2} e^{x'/L_{\rm P}}$$

$$L_{\rm P} = \sqrt{D_{\rm P}\tau_{\rm p}}$$

• L<sub>P</sub> : hole minority carrier diffusion length

#### **Excess Carrier Distribution**

$$\Delta p_{\mathrm{n}}(x') = A_{\mathrm{l}}e^{-x^{\prime}/L_{\mathrm{P}}} + A_{\mathrm{2}}e^{x^{\prime}/L_{\mathrm{P}}}$$

New boundary conditions

$$\Delta p_{\rm n}(x' \to 0) = p_{\rm n0}(e^{qV_{\rm A}/kT} - 1)$$
$$\Delta p_{\rm n}(x' \to \infty) = 0$$

From the 
$$x' \to \infty$$
,  $A_2 = 0$   
From the  $x' \to 0$ ,  $A_1 = p_{n0}(e^{qV_A/kT} - 1)$ 

$$\Delta p_{\rm n}(x') = p_{\rm n0}(e^{qV_{\rm A}/kT} - 1)e^{-x'/L_{\rm P}}, \ x' \ge 0$$

Similarly,

$$\Delta n_{\rm p}(x'') = n_{\rm p0}(e^{qV_{\rm A}/kT} - 1)e^{-x''/L_{\rm N}}, \ x'' \ge 0$$

### pn Diode I–V Characteristic

**n-side** 
$$\mathbf{J}_{P}(x') = -qD_{P} \frac{d\Delta p_{n}(x')}{dx'} = q \frac{D_{P}}{L_{P}} p_{n0} (e^{qV_{A}/kT} - 1)e^{-x'/L_{P}}$$

**p-side** 
$$\mathbf{J}_{N}(x'') = -qD_{N} \frac{d\Delta n_{p}(x'')}{dx''} = q \frac{D_{N}}{L_{N}} n_{p0} (e^{qV_{A}/kT} - 1)e^{-x''/L_{N}}$$

$$\mathbf{J} = \mathbf{J}_{\mathrm{N}} \big|_{x = -x_{\mathrm{p}}} + \mathbf{J}_{\mathrm{P}} \big|_{x = x_{\mathrm{n}}} = \mathbf{J}_{\mathrm{N}} \big|_{x'=0} + \mathbf{J}_{\mathrm{P}} \big|_{x'=0}$$

$$\mathbf{J} = q n_{\rm i}^2 \left( \frac{D_{\rm N}}{L_{\rm N} N_{\rm A}} + \frac{D_{\rm P}}{L_{\rm P} N_{\rm D}} \right) (e^{q V_{\rm A}/kT} - 1)$$

#### *pn* Diode *I*–*V* Characteristic



$$I = A\mathbf{J} = Aqn_{i}^{2} \left(\frac{D_{N}}{L_{N}N_{A}} + \frac{D_{P}}{L_{P}N_{D}}\right) (e^{qV_{A}/kT} - 1)$$

$$I = I_0 (e^{qV_A/kT} - 1)$$
$$I_0 = Aqn_i^2 \left(\frac{D_N}{L_N N_A} + \frac{D_P}{L_P N_D}\right)$$

- Shockley Equation, for ideal diode
- *I*<sub>0</sub> can be viewed as the drift current due to minority carriers generated within the diffusion lengths of the depletion region

#### Diode Saturation Current $I_0$

$$I_{0} = Aqn_{i}^{2} \left( \frac{D_{P}}{L_{P}N_{D}} + \frac{D_{N}}{L_{N}N_{A}} \right)$$

I<sub>0</sub> can vary by orders of magnitude, depending on the semiconductor material, due to n<sup>2</sup> factor.

In an asymmetrically doped *pn* junction, the term associated with the more heavily doped side is negligible.

If the p side is much more heavily doped,

$$I_0 \cong Aqn_i^2 \left(\frac{D_{\rm P}}{L_{\rm P}N_{\rm D}}\right)$$

If the *n* side is much more heavily doped,

$$I_0 \cong Aqn_i^2 \left(\frac{D_N}{L_N N_A}\right)$$

#### **Diode Carrier Currents**



#### **Carrier Concentration: Forward Bias**



#### Carrier Concentration: Reverse Bias

Deficit of minority carriers near the depletion region.

Depletion region acts like a "sink", draining carriers from the adjacent quasineutral regions



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#### Breakdown Voltage, $V_{\rm BR}$

If the reverse bias voltage (−V<sub>A</sub>) is so large that the peak electric field exceeds a critical value E<sub>CR</sub>, then the junction will "break down" and large reverse current will flow.

$$\boldsymbol{\mathcal{E}}_{CR} = \sqrt{\frac{2q}{\mathcal{E}_{S}} \left(\frac{N_{A}N_{D}}{N_{A} + N_{D}}\right) \left(V_{bi} + V_{BR}\right)} \bullet \text{At breakdown, } \boldsymbol{V}_{A} = -\boldsymbol{V}_{BR}$$

Thus, the reverse bias at which breakdown occurs is

$$V_{\rm BR} = \frac{\varepsilon_{\rm S} \varepsilon_{\rm CR}^{2}}{2q} \left( \frac{N_{\rm A} + N_{\rm D}}{N_{\rm A} N_{\rm D}} \right) - V_{\rm bi}$$

#### Breakdown Mechanism: Avalanching



#### Breakdown Mechanism: Zener Process





Barrier must be thin breakdown mechanism when both junction sides are heavily doped.

Potential energy

barrier

Typically, Zener process dominates when  $V_{BR} < 4.5V$  in Si at 300K and  $N > 10^{18}$  cm<sup>-3</sup>.



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# **Chapter 7** *pn* Junction Diodes: Small-Signal Admittance

### Small-Signal Diode Biasing

- When reversed-biased, a pn junction diode becomes functionally equivalent to a capacitor, whose capacitance decreases as the reverse bias increases.
- Biasing additional a.c. signal v<sub>a</sub> can be viewed as a small oscillation of the depletion width about the steady state value.



Chapter 7 pn Junction Diodes: Small-Signal Admittance

#### Total *pn* Junction Capacitance



$$C_{\rm J} = A \frac{\mathcal{E}_{\rm s}}{W}$$
  
Minority  
carrier  
lifetime 
$$C_{\rm D} = \frac{\tau I_{\rm DC}}{kT/q}$$

Junction / depletion capacitance, due to variation of depletion charges

#### Diffusion capacitance,

due to variation of stored minority charges in the quasineutral regions

- C<sub>J</sub> dominates at low forward biases, reverse biases.
- $C_{\rm D}$  dominates at moderate to high forward biases.

### Relation Between $C_{\rm J}$ and $V_{\rm A}$

For asymmetrical step junction,

$$W = \sqrt{\frac{2\varepsilon_{\rm s}}{qN_{\rm B}} (V_{\rm bi} - V_{\rm A})}$$

 $N_{\rm B}$  : bulk semiconductor doping,  $N_{\rm A}$  or  $N_{\rm D}$  as appropriate.

#### Therefore,

$$\frac{1}{C_{\rm J}^{2}} = \frac{W^{2}}{A^{2} \varepsilon_{\rm s}^{2}} \cong \frac{2}{q N_{\rm B} \varepsilon_{\rm S} A^{2}} (V_{\rm bi} - V_{\rm A})$$

- A plot of  $1/C_{J^2}$  versus  $V_A$  is linear.
- The slope is inversely proportional to  $N_{\rm B}$ .
- An extrapolated  $1/C_J^2 = 0$  intercept is equal to  $V_{bi}$ .